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Report No. 8926-085

Materials - Alloy Steel - Ultra-High Strength H-ll Hot Work Die Steel - Vascojet 1000 (Vanadium Alloy Steel Co.)

Rivet Shear Strength and Corrosion Resistance

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Rivet Shear Strength and Corrosion Resistance

Abstracc

Annealed Vascojet 1000 steel (Vanadium Alloy Steel Co., Latrobe, Penna.) rivets were cold headed from 1/8 and 1/4 inch diameter rivet wire and then heat treated. The heat treatment consisted of 1800°F for 30 minutes, air cool, 1150°F for 1-1/2 hours, air cool, 1150°F for 1-1/2 hours, air ccol. The ultimate tensile strength after heat treatment of the 1/8 and 1/4 inch diameter wire was 200.7 and 191,4 ksi, respectively. Tandem protruding head rivets spaced at 4 rivet diameters, held to 2 rivet diameter minimum edge distance, and driven to head diameters about 1.5 times shank diameters were driven into 0.125 inch thick clad 7075-T6 aluminum alloy sheet lap shear joints and tested. In these tests the 1/8 inch diameter rivets yielded (0.005 inch offset) at 1638 pounds and failed at 1765 pounds with an ultimate strength of 136.2 ksi, and the 1/4 inch diameter rivets yielded (0.00625 inch offset) at 5767 pounds and failed at 6275 pounds with an ultimate strength of 121 ksi. Salt spray corrosion tests with riveted joints indicated that corrosion damage to clad 7075-T6 sheet is accelerated by the presence of unprotected Vascojet 1000 steel rivets.

Reference: Stier, H. H., Bergstedt, P. W., Turner, H.C.,
"Mechanical & Corrosion Properties of Vascojet
1000 Rivets," General Dynamics/Convair Report
MF 58-238, San Diego, California, 2 February
1959. (Reference attached.)

STRUCTURES & MATERIALS LABORATORIES

REPORT MP 58-238

DATE 2 February 1959

MODEL REA 7038

A DIVISION OF GENERAL DINAMICS CORPORATION

SAN DIEGO

TITLE

REPORT NO. MP 58-238

MECHANICAL & CORROSION PROPERTIES
OF VASCOJET 1000 RIVETS

MODEL: REA 7038

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C O N V A I R

ANALYSIS
PREPARED BY H. Stier
CHECKED BY Bergstedt/Turner/Sutherland

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MODEL REA 7038
DATE 2-2-59

OBJECT:

To determine (a) the strength and driving characteristics, and (b) the corrosive effect of <u>VASCOJET 1000</u>* rivets in 7075-T6 aluminum alloy sheet.

CONCLUSION:

- 1. The shear strength of double-tempered <u>VASCOJET 1000</u>* wire increases parabolically with increasing hardness of the wire in the range from 42-51 Rockwell C (when tested at room temperature in a double-shear fixture).
- 2. Lapped joints in bare 7075-T6 sheet fastened by double-tempered <u>VASCOJET 1000</u> rivets of 42-44 Rc hardness with protruding flat heads have these strengths (when tested at room temperature):

1/8" diam. rivets 1/4" diam. rivets in .125" thk. sheet in .250" thk. sheet

Ultimate shear, psi

136,200

121,000

- 3. <u>VASCOJET 1000</u> wire double-tempered to 42-44 Rc hardness has an ultimate tensile strength of 191,000 201,000 psi.
- 4. The force required to squeeze a .337 ± .005 in. diameter head on a .250 in. diameter <u>VASCOJET 1000</u> rivet varies with the hardness.

Rivets of Rivets of 44 Re hardness 50 Re hardness

Rivet-driving force, pounds

23,400

28,400

- 5. Rivet heads squeezed to .337 ± .005 in. diameter on .250 in. diameter <u>VASCOJET 1000</u> rivets of 42-51 Rockwell C hardness show no rejectable cracks.
- 6. Corrosion in clad 7075-T6 sheet is accelerated by the bare <u>VASCOJET 1000</u> rivets.

TEST SPECIMENS:

Rivets were cold-headed from <u>VASCOJET 1000</u> wire in the annealed condition and then heat-treated as follows:

- a. Austenitize at 1850°F. in a neutral atmosphere for 30 sinutes, air cool.
- VASCOJET 1000 is Vanadium-Alleys Steel Company's designation for an AISI-Hil steel.

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ANALYSIS PREPARED BY Stier REVISED BY

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TEST SPECIMENS: (Continued)

- b. Temper at 1150°F. in air for 1 1/2 hours. air cool.
- c. Temper again at 1150°F. in air for 1 1/2 hours, air cool.

The 1/8 in. diameter rivets were squeezed with a Chicago Pneumatic compressriveter; the 1/4 in. diameter rivets were gunned with a G-8 pneumatic rivet gun. Rivet shanks protruded 1.12 diameters before driving in the sheet combinations of this test.

The shear specimens were of the single lap-joint type with two tandem rivets spaced along the longitudinal center-line of the joint as shown in the sketch in Table I. Corrosion specimens had three driven rivets spaced at one inch along the lengitudinal center-line of $.125^{\circ}$ x 1 $1/2^{\circ}$ x 10° clad 7075-T6 sheet.

TEST PROCEDURE:

The riveted lap-joints were pulled in a 60,000 pound Timius-Olsen tensile machine at a maximum loading rate of 1000 pounds/min. for 1/8 in. diameter rivets and 4000 pounds/min. for 1/4 in. diameter rivets. An S-1 extensometer was used to measure the yield strength of the joint as described in Report MP 58-262. The yield load was taken at a permanent joint set of .005 in. for 1/8 in. diameter rivets and .00625 in. for 1/4 in. diameter riveta.

Tensile specimens of 15 in. lengths of wire were inserted into 1/8 in. or 1/4 in. I.D. javs and pulled at .001 in./in./min. to determine the tensile ultimate of the wire. The I.D. of the jave was smooth to prevent notehing of the wire. An abrasive coating on the ends of the wire was needed to overcome slipping in the javs.

Shear tests of tempered wire were performed in a double-shear fixture. Before shearing the wire, the hardness was taken along the diameter of a polished and etched cross-section through the wire. Vickers hardnesses were measured with a diamond pyramid indenter in a Tukon tester with a 10 Kgm. load. The specimen was broken out of its lucite mount before measuring the Rockwell C hardness of the cross-section.

The corrosion specimens were wiped wit. alcohol and placed in a salt spray cabinet for observation. The salt spray was operated in accordance with Federal Test Method Standard 151, Nethod 811.

RESULTS & DISCUSSION:

The heat treatment for VASCOJET 1000 rivets for this test was selected on the basis of the double-shear tests of wire tempered to different hardnesses. (See Figure 1). A shear strength of 139,000 psi. was achieved by tempering to about 44 Rc hardness. Two different double-tempering treatments which produced a 44 Rc hardness are given below:

a. 1100°F., 2 1/2 hours, AC + 1100°F., 2 1/2 hours, AC.

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RESULTS & DISCUSSION: (Centimued)

b. 1150°F., 1 1/2 hours, AC + 1150°F., 1 1/2 hours, AC.

NOTE: An austenitizing treatment at 1850°F. in a neutral atmosphere for 30 minutes, followed by air cooling, put the material in a fully hardened condition before double-tempering.

The 139,000 psi ustimate shear strength was selected so that failure would eccur in the rivets before the bearing strength of the bare 7075-T6 sheet was exceeded

No sheet bearing failures occurred in tests of lapped joints in 7075-T6 sheet incorporating VASCOJET 1000 rivets of 42-44 Rc hardness. (See Table I.)

The ultimate tensile strength of <u>VASCOJET 1000</u> wire of 42-44 R_c hardness is given in Table II.

The load required to squeeze the protruding heads of the 1/4 in. diameter VASCOJET 1000 rivets to .337 : .005 in. diameter is given in Table III. Driven heads showed very minute surface cracks (not rejectable according to MPS-46.05D).

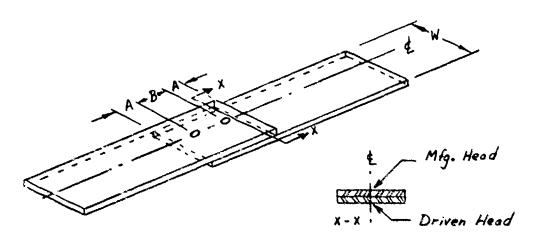
The corrosion specimen incorporating VASCOJET 1000 rivets in clad 7075-T6 sheet was severely attacked after 250 hours in the salt spray cabinet. The cladding was completely removed in areas up to one inch in diameter near each rivet head. Rivet heads showed no corresion. Coatings of diffused or plated metals on the VASCOJET 1000 rivets may be applied for pretection against corrosion.

"Steels and Protective Treatments for Use up to 1000 F.. " H. J. Alle and W. H. Sharp, SAE Transactions, Volume 64, 1956, pt. 74-75.

The data for this report have been recorded in the Materials and NOTE: Processes Laboratory Notebook No. 3011.

TABLE I. RESULTS OF SHEAR TESTS OF RIVETED LAP-JOINTS INCORPORATING PROTRUDING HEAD RIVETS OF TEMPERED (a) VASCOJET 1000 (b) STEEL IN 7075-T6 SHEET (bare).

Identif.	Driving		Driven Head Diam.,in.	Thk.,		ULT. LOAD #/rivet	ULT. STRENGTH, PSI. (c)	TYPE OF FAILURE (d)
V J- 1	G-8 gun	-257258	.347362	-250	5637	5950	114,800	1 & 2
VJ-2	4 2 2	.257	.356369	H	5650	6300	121,400	2
VJ-3	11	-	.353359	Ħ	6013	6575	126,800	1 & 2
		Q Q		Avg.	5767	6275	121,000	
VJ -4	Squeeze	.1285	.180	.125	1595	1720	132,600	2
VJ-5	H	Ħ	.176181		1605	1735	134,000	2
VJ-6	10	n	.177178	**	1715	1840	142,000	2
					1638	1765	136,200	



	SPECIMEN	DIMENS:	IC'S:	
Shoot	Civot Diam	A	8	w
in.	in.	in.	in-	in.
.135 .250	1/8 1/4	1/2 5/8	3/4 1	1 1/0 1 1/2

- (a) Rivots were tempered to a Rockvoll hardness of 42 44 Ro before driving (1850° F., 30 min., AC + 1150° F., 1 1/2 hr., AC + 1150° F., 1 1/2 hr., AC).
- (b) Vanadium-Alloys Steel Company's designation for an AISI-Hil steel.
- (c) Based on measured hole diameter.
- (d) See FAILURE NOTES belows
 - 1. Mfg. heads snapped off.
 - 2. Rivets sheared in the shank along sheet interface.

TABLE II. RESULTS OF TENSILE TESTS OF TEMPERED(a) VASCOJET 1000 (b) RIVET WIRE

Wire Diam. inch	Area, in.2	Longth, inch		ULT. LOAD, pounds	ULT.	TENSILE PSI.	STRENGTH,
.1258	.012425			2520		202,898	
•	**	**		2470		198,872	
	19	19		2490		200,483	
			Avg.	2493		200,751	
.2505	.04926	15		9370		190,215	
.2503	.C4918	W		9570		194,591	
tt	**	th		9320		189,507	
			Avg.	9420		191,438	

⁽a) Wire tempered to a Rockwell hardness of 42 - 44 R_c (1850° F., 30 min., AC + 1150° F., 1 1/2 hr., AC + 1150° F., 1 1/2 hr., AC).

⁽b) Vanadium-Alloy: Steel Company's designation for an AISI-Hill steel.

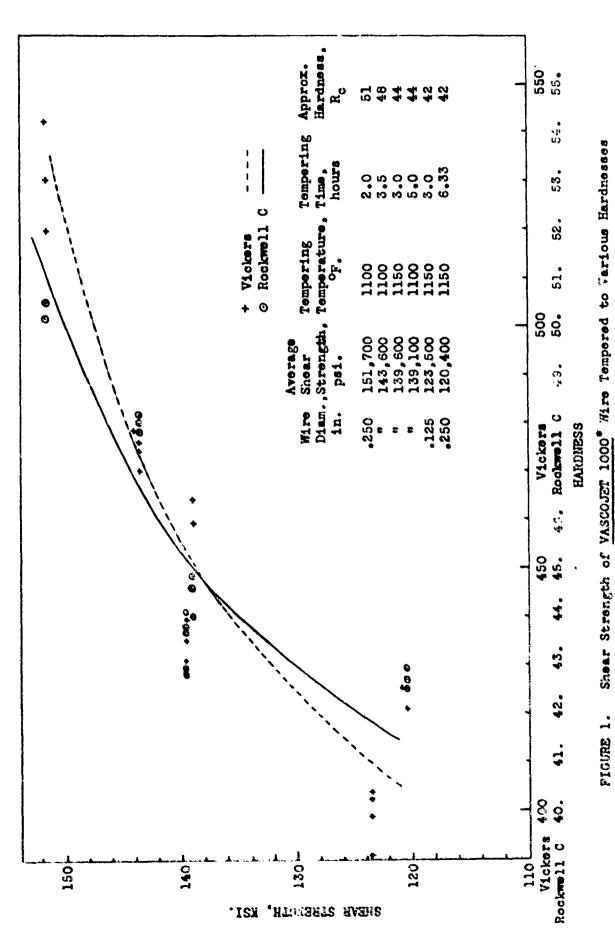
TABLE III. RESULTS OF RIVET-DRIVING TESTS OF TEMPERED (c) VASCOJET 1000 (a) RIVETS IN 7075-T6 SHEET (bare)

Rivet Diam., in.	Hole Diam., in.	Driven Head Diam., in.	Sheet Thk., in.	Rivet Set	Rivet Hardness, R _C		D REQUIRED SQUEEZE RIVET, pounds	Remarks
-250	.257	.3356	•125	Flat	42-43		20,400	(b)
-5	#	.3392	19	**	11		21,600	W
18	19	.3408	11	17	Ħ		21,800	Ħ
						Avg.	21,300	
. 250	.257	.3349	•125	Flat	43-44		23,600	(b)
**	Ħ	.3409	22	19	19		21,600	W
17	**	.3415	•	*	19		25,000	t#
						Avg.	23,400	
.250	.257	.3327	.125	Flat	44-45		22,300	(b)
#	17	.3356	**		79		22,800	'n
17	•	.3366	*	. 18	w		23,200	w
						A▼g.	22,800	
.250	.257	.3350	.125	Flat	50-51		28,300	(b)
•	*	.3366	73	Ħ	•		27,800	`₩
ti	17	.3416	10	w	•		29,150	u
		•				Avg.	28,400	

⁽a) Vanadium-Alloys Steel Company's designation for an AISI-Hll steel.

⁽b) Driven heads showed very minute surface cracks about .010" long and a few mils deep.

⁽c) Tempered to the hardnesses indicated in column 6 before driving.



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FIGURE 1.

Vanadium-Alloys Steel Company's designation for an AISI-HII steel. Composition: 0.40 % C, 5.0 % Cr, 1.30 % No, 0.50 % V.